

*Supplemental Amendment dated September 23, 2003  
Reply to Final Office Action dated May 21, 2003*

*Serial No. 09/840,040  
Docket No. 1781-224P  
Group Art Unit 2834  
Page 3*

**CLAIM SET AS AMENDED:**

1. (Currently Amended) A control system for controlling a plant having an operating characteristic which describes the translation of a plant input to a plant output, wherein the plant operating characteristic has a linear component and a non-linear component, the control system comprising:

a feedback control function; and

a feed-forward control function,

wherein a demand signal is simultaneously applied to respective inputs of the feedback and feed-forward control functions, and respective outputs of the feedback and feed-forward control functions are summed together to generate the plant input, the feed-forward control function having a first component which is a function of a model of the linear component of the plant characteristic, and a second component which is an adaptive function to compensate for the non-linear component of the plant characteristic, the adaptive function being substantially modeled on the non-linear component of the plant characteristic and having adaptive laws which vary parameters of the adaptive function with time such that the adaptive function approaches the non-linear component of the plant characteristic, and

wherein the plant is a permanent magnet linear motor (PMLM) wherein the feedback control function is a Proportional/Integral/Derivative (PID) controller.

2. (Currently Amended) The control system of claim 1 wherein the non-linear component of the plant characteristic is of the form:

*Supplemental Amendment dated September 23, 2003  
Reply to Final Office Action dated May 21, 2003*

*Serial No. 09/840,040  
Docket No. 1781-224P  
Group Art Unit 2834  
Page 4*

$$u_{ripple} = A(x)\sin(\omega x + \emptyset) = A_1(x)\sin(\omega x) + A_2(x)\cos(\omega x),$$

where  $x$  is the plant variable,

and where the adaptive function has the form:

$$u_{AFC} = a_1(x(t))\sin(\omega x) + a_2(x(t))\cos(\omega x),$$

where

$$\dot{a}_1(x(t)) = -ge\sin(\omega x), \quad \dot{a}_1(t) = -ge\dot{x}_d \sin(\omega x),$$

$$\dot{a}_2(x(t)) = -ge\cos(\omega x), \quad \dot{a}_2(t) = -ge\dot{x}_d \cos(\omega x),$$

$e$  is an error signal given by:

$$e = (x_d - x),$$

$g$  is an adaptation gain and is greater than 0,  $x_d$  is the desired function of the plant variable and  $\omega$  is related to 1/period of the non-linear component of the plant characteristic, such that the adaptive feed-forward control function continuously adjusts the parameters  $a_1$  &  $a_2$  in response to the error signal  $e$ .

3. (Previously Presented) The system of claim 2, wherein the plant variable  $x$  represents an instantaneous position of a translator of the linear motor, the desired function of the plant variable  $x_d$  represents the desired trajectory of the translator and the PMLM has a magnetic structure having a pole pitch  $x_p$ , such that  $\omega = 2\pi / x_p$ .

4. (Currently Amended) The system of claim 3 wherein the adaptation gain has a value which is greater ~~that~~ than zero and less than or equal to one.

*Supplemental Amendment dated September 23, 2003*  
*Reply to Final Office Action dated May 21, 2003*

*Serial No. 09/840,040*  
*Docket No. 1781-224P*  
*Group Art Unit 2834*  
*Page 5*

5. (Original) The system of claim 4 wherein the adaptation gain has a value which is less than 0.6.

6. (Original) The system of claim 5 wherein the adaptation gain has a value which is greater than or equal to 0.2.

7. (Original) The system of claim 6 wherein the adaptation gain is equal to 0.2.

8. (Canceled)